

Technical Appendix 2.2: Borrow Pit Assessment

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1.1 Introduction

- 1.1.1
- To reduce the volume of imported aggregate transported and any consequent environmental impacts, borrow pits are to be located within the Site (defined by the application boundary on **Figure 2.1: Site Layout (EIAR volume 3a)**), subject to further geotechnical evaluation, to source aggregate required for track construction, turbine bases, crane pads, compounds and hardstanding areas. This report provides details of the proposed on-site borrow pits for use during the construction phase of the Proposed Development. One potential borrow pit location has been identified. The Proposed Development is described in **Chapter 2: Proposed Development (EIAR Volume 2)** and the proposed borrow pit search areas are shown on **Figure 2.2.1: Borrow Pit Location Plan** (in this Technical Appendix). **Section 1.4** of this report provides specific information about the borrow pit search areas and restoration details.
- 1.1.2
- The Proposed Development is a renewable energy development comprised of up to eight wind turbines, a Battery Energy Storage System (BESS) and associated infrastructure adjacent to Sullom Voe Oil Terminal (SVT) and the Shetland Gas Plant in Shetland, Scotland.

Aims of this Report

- 1.1.3
- This report provides geo-engineering information on the potential for a borrow pit that would be opened within the Site. The aim of this assessment is to provide:
 - a preliminary indication of the suitability of the bedrock as construction material;
 - potential borrow pit locations;
 - indicative borrow pit dimensions;
 - indicative extraction volumes;
 - estimates of overburden volumes borrow pit locations;
 - an indication of potential extraction methods;
 - recommendations for geotechnical testing; and
 - preliminary borrow pit re-instatement and rehabilitation proposals.
- 1.1.4
- This report outlines the methodology used by Ramboll for borrow pit assessment along with the analysis undertaken; conclusions drawn and recommendations for the proposed borrow pit design.

Limitations

- 1.1.5
- It should be noted that all borrow pit information provided within this report is indicative only and is based on desk study and reconnaissance of the Site alone. No intrusive investigation (other than peat probing) has been carried out and consequently the suitability of the rock, suggested extraction methods and volumes are broad estimates and should be treated as such. A detailed ground investigation (such as boreholes and trial pits) would be required to determine the suitability of the rock (extent and quality), potential for groundwater ingress and to determine geotechnical parameters. Recommendations can then be made with regards to groundwater control, slope stability, extraction methods and finalised detailed design. The search areas have been identified for a borrow pit to allow

for any adjustments following the results of the ground investigation. The final dimensions of the borrow pit are likely to be significantly different to the individual search areas (i.e. they will be smaller).

- 1.1.6
- This report represents the findings and opinions of experienced geotechnical consultants based upon the information obtained from a variety of sources as detailed below. Ramboll believes the information obtained from third parties is reliable but does not guarantee its authenticity. The information has been accepted *de facto* but professional judgement has been used in its interpretation.

1.2 Methodology

- 1.2.1
- This report comprises a desk-based study and notes compiled from a geo-engineering walkover survey. The desk study consisted of a review of the available geological and hydrogeological data together with additional information relating to the Site including:
 - 1:50,000 and 1:25,000 scale Ordnance Survey (OS) topographic mapping;
 - OS Elevation Digital Terrain Mapping (DTM) data;
 - review of geological mapping for the Site, British Geological Survey (BGS)¹ 1:50,000 scale;
 - review of publicly available aerial photography and OS aerial imagery;
 - groundwater vulnerability map of Scotland²;
 - BGS 1:625,000 scale hydrogeological map³;
 - review of peat probe survey field data; and
 - a site walkover to identify suitable borrow pit locations.
- 1.2.2
- Two walkover surveys have been undertaken within the Site. The first survey was undertaken in April 2025. Following the initial survey observations, two borrow pit search areas were initially identified. The borrow pit search areas were subsequently investigated during the second walkover survey undertaken in July 2025.
- 1.2.3
- During the post survey design process the initial two borrow pit locations were reduced to one proposed location that is discussed in detail within the sections below and form part of the Proposed Development.
- 1.2.4
- All survey work recorded detailed field notes and photographs of the potential borrow pit sites, including details of the geological and hydrogeological aspects of each identified location. A hand-held GPS was used to determine the grid reference.
- 1.2.5
- The suitable borrow pit location has been considered in more detail in the sections below. A preliminary borrow pit layout within this location has been provided alongside a calculation of the estimated volume of material which could be extracted. This is discussed in more detail in subsequent sections.
- ### Borrow Pit Constraints
- 1.2.6
- One of the principal factors affecting borrow pit location is the thickness of overburden material, due to the increased effort required for its excavation and handling before the source of the aggregate is reached. Therefore, this assessment has sought to identify optimal borrow pit locations where there would be no, or only a very thin veneer of superficial deposits, especially peat (due to its high moisture content and broader environmental considerations).

¹ British Geological Society BGS Geo Index mapping Available: <https://mapapps2.bgs.ac.uk/geoindex/home.html> [Accessed 05/02/2026]

² Scottish Environment Protection Agency *flood map*. Available: <http://map.sepa.org.uk/floodmap/map.htm> [Accessed 05/02/2026]

³ British Geological Survey, *1:625,000 scale digital hydrogeological data*. Available: <http://www.bgs.ac.uk/products/hydrogeology/maps.html> [Accessed 05/02/2026]

- 1.2.7 In addition, the borrow pit assessment has sought to avoid areas of high groundwater table in order to reduce the potential for dewatering of the borrow pit excavation. In doing so, the potential borrow pit locations also reduce the potential for erosion and additional processes required for handling and treatment of groundwater. At this stage groundwater mitigation measures, including an application for an Environmental Authorisation (Scotland) Regulations (EASR) Permit ⁴, are considered not to be required. Groundwater levels within the proposed borrow pit search areas will be confirmed as part of the findings from detailed ground investigation.
- 1.2.8 The borrow pit location has also been selected to avoid existing watercourses due to the potential for runoff of sediment and fine grained material.
- 1.2.9 Consideration is also given to the potential for visual effects and impacts on the setting of cultural heritage features; however it is considered that, with sensitive development and appropriate restoration, long term significant effects associated with borrow pits can be avoided.

1.3 Desk Study and Site Information

- 1.3.1 The Site location and setting are described within **Chapter 2: Description of Proposed Development (EIAR Volume 2)**.

Topography

- 1.3.2 The topography of the northern extents of the Site is generally undulating rising from mean high water level of Yell sound to 116 m above Ordnance Datum (AOD) at the summit of Hill of Crooksetter. The southern extents of the Site gently undulate between levels of 40 m AOD and 90 m AOD. Topography elevations are shown on **Figure 8.6.1, Technical Appendix 8.6: Peat Landslide Risk Assessment (EIAR Volume 4)**.

Superficial Geology

- 1.3.3 The 1:50,000 scale geological mapping available from the British Geological Survey (BGS)¹ shows the superficial geology across the majority of the Site is predominantly peat. Isolated areas of Quaternary aged, Devensian, Till – Diamicton are shown to be present across the Site. NatureScot Carbon and Peatland mapping⁵ also shows peat to be present across virtually all of Site, with the exception of an area located to the southwestern extents. The mapping shows the peat to be Class 1 peatland and designated as '*Nationally important carbon rich soils, deep peat and priority habitat*'.
- 1.3.4 Peat probing undertaken in 2025 confirmed the presence of peat across the vast majority of the Site. The findings of the survey are presented within **Technical Appendix 8.4: Peat Depth Survey Results (EIAR Volume 4)**.
- 1.3.5 The depth of superficial deposits was taken into account when selecting potential borrow pit locations, typically avoiding areas with >0.5 m peat or other superficial deposits. A maximum depth of 0.5 m of peat was observed at the proposed borrow pit location. As discussed in Section 1.2 above, one borrow pit search area was excluded following the phase 2 survey, due to peat being present up to a depth of 1.8 m. The remaining borrow pit location is assumed to have an overburden of less than 0.5 m assumed for design.

Bedrock Geology

- 1.3.6 The 1:50,000 scale geological mapping available from the British Geological Survey (BGS)¹ shows the north eastern, central and southern regions of the Site to be underlain by early Devonian-aged Graven Complex Formation rock (Granodiorite). Granodiorite is a coarse-grained (phaneritic) intrusive igneous

rock. The north western extents of the Site are underlain by metamorphic rocks of the Tonian aged, Yell Sound Psammite formation (psammite and pelite). The formation comprises psammite, variably gneissose; with subsidiary layers or lenses of amphibolite, pelite, quartzite and gneissose semipelite. The proposed borrow pit location is located within the Igneous Graven Complex formation rocks.

Structural Geology

- 1.3.7 BGS mapping¹ shows two major fault lines, approximately 4.6 km to the east (Nesting Fault) and 5 km west (Walls Boundary Fault) of the Site. Both faults are running approximately in a north to south direction.

Hydrology

- 1.3.8 The BGS 1:625,000 scale hydrogeology mapping³ defines the rocks as follow:
- Graven Complex Formation = low productivity aquifer (limited groundwater in near surface weathered zone and secondary fractures).
 - Yell Sound Psammite Formation = Low productivity aquifer (small amounts of groundwater in near surface weathered zone and secondary fractures; rare springs).

Surface Water Features

- 1.3.9 The northern extents of the Site comprises an undulating plateau that ranges in elevation from mean high-water level at its northernmost extent by Ay Wick, to 116 m AOD at the Hill of Crooksetter located in the centre of the Site. The northern extent of the Site primarily drains into the Aywick Burn flowing in a north westerly direction and the Burn of Toft flowing eastwards. A small section of Burn of Crooksetter and its tributaries are located in the west of the Site. A section of Neshion Water is located in the east of the Site. The Site is bounded in the northwest by Yell Sound (coastal waterbody).
- 1.3.10 Towards the southern end of the Site, the topography gently undulates between 40 m AOD and 90 m AOD. The slackness of slopes in this part of the Site is associated with a number of lochans including Sand Water, Nugla Water and the Loch of Bordigarth and their connecting watercourses. Tributaries from the Burn of Laxobigging are also located in the south of the Site.
- 1.3.11 The borrow pit search area has been selected to avoid borrow pit extraction within 50 m of existing watercourses or waterbodies and with standard mitigation (i.e. an upslope cut-off/diversion ditch to intercept surface water together with minor attenuation features or soakaways) the borrow pits are not considered likely to have any significant effect on surface water.

Suitability of Bedrock within the Site as an Aggregate

- 1.3.12 The Site is predominantly underlain by igneous and metamorphic rock formations rock, predominately comprising granodiorite and psammite (metasandstone) and metamudstone, described as being largely medium to coarse grained. Granodiorite is assumed to be present at the proposed borrow pit location, based on BGS mapping¹.
- 1.3.13 Granodiorite is known for its high strength and high resistance to weathering and displays excellent wear resistance when used as a construction aggregate.
- 1.3.14 Should psammite rocks be present within the borrow pit search area, then this would also be suitable for reuse, with psammite being a metasandstone. Sandstone is widely used as a construction aggregate and foundation material. However, it should be noted that psammite is far more prone to weathering than igneous rock formations. It is also noted that the Yell Psammite formation may also be interbedded

⁴ Scottish Government. (2018) The Environmental Authorisations (Scotland) Regulations 2018. [online] Available from: <https://www.legislation.gov.uk/sdsi/2018/9780111039014/contents> [Accessed 10/03/2026]

⁵ NatureScot (2016) *Carbon & Peatland mapping* [online] Available from: https://map.environment.gov.scot/Soil_maps [Accessed 05/02/2026]

with pelite rock (metamudstone) which may have the potential to increase fine material content when processed.

- 1.3.15
- A rocks suitability as aggregate largely depends on its strength, porosity and durability, which are in turn governed by characteristics such as mineralogical composition, grain size and sorting, cementation and weathering state.
- 1.3.16
- A key factor in the suitability of the rock as aggregate is the mineral constitution and mode of occurrence, as often their quality is not uniform. The weathering state of the rock is also of high importance, as this weakens the aggregate and reduces durability. The depth of weathering is dependent on the distribution of joints and other rock discontinuities.
- 1.3.17
- No rock formations were observed within the borrow pit search area during the walkover surveys. Therefore, the rock type, discontinuity spacing and bedding orientation cannot be verified at this stage. A rock type and weathering profile will be assumed for the purposes of this assessment based on the desk study information above.
- 1.3.18
- The proposed borrow pit locations would need detailed investigations to verify rock type and quality, bedding orientation and weathering profile to minimise extraction of unsuitable or argillaceous material with a potential for high fines content after excavation/grading.

1.4 Borrow Pit Locations and Restoration Details

- 1.4.1
- The proposed borrow pit search area has been selected based on a preferential morphology for stone extraction (limited cover, rock close to surface and moderately steep slopes). The proposed borrow pit location has been sited to avoid areas with >0.5 m peat or other significant depths of superficial deposits. The locations also take into account visual, ecological, hydrological and cultural heritage constraints. The search areas identified allow for any adjustments following the results of the ground investigation. The borrow pits are likely to be smaller in size relative to the search areas.
- 1.4.2
- The borrow pit has been located with the aim of providing an area of site-won rock within the Site, in an effort to minimise transportation of aggregate.
- 1.4.3
- The preliminary estimation of potential material quantities which could be extracted from the proposed borrow pit location is provided in **Table 2.2.1**. The volumes given have been calculated from 3D modelling of the borrow pits assuming all extraction is undertaken from a single layer or ‘bench’, taking into account gradients of the ground surface and the indicative borrow pit footprint dimension and depth approximations. Please note that these figures do account for a 20% reduction due to wastage (associated with highly weathered material) or bulking of excavated materials.
- 1.4.4
- No account has been taken in the calculations for ‘winning’ rock during the construction phase (e.g. through track and turbine base excavations and widening of the existing track). The extent of material sourced in this manner would minimise the extraction of rock from the borrow pits.
- 1.4.5
- Overburden/soils together with processing residue would be carefully stockpiled adjacent to the excavation void for use in the borrow pit restoration process. The stockpiles would be located and battered so as to limit instability and erosion. Silt fences and mats would be used to minimise sediment levels in runoff from the stockpiles.
- 1.4.6
- It is anticipated that, upon completion, the borrow pits would be partially reinstated. This would involve the reworking of faces to stabilise them, partial infilling with site-won material and landscaping with soils excavated during construction of the Proposed Development. There would also be the potential for environmental enhancement by creating small wetlands or other desirable habitats, further details of which are set out within the outline Biodiversity Enhancement and Habitat Management Plan (**Technical**

Appendix 6.5: Outline Biodiversity Enhancement and Habitat Management Plan (OBEHMP) (EIAR Volume 4)).

- 1.4.7
- Borrow pit restoration would utilise processing residues and overburden and would create slopes within the excavation at an approximate gradient of 2 (V) in 1 (H). The crest of the slopes would intersect the uppermost rock face at a position which partially obscures the lower part of the faces. The toe of the restoration faces would be blended in to the borrow pit floor, which itself would be re-profiled to allow drainage and the re-introduction of appropriate cover. The upper part of the borrow pit faces would remain exposed and would be allowed to become weathered. It is envisaged that this face would acquire an appearance similar to that of other natural rock exposures in the locality.

Borrow Pit Details

- 1.4.8
- An indicative borrow pit design has been prepared for the proposed borrow pit search area, and includes the following details and assumptions:
 - the footprint area of the excavation for the proposed borrow pit;
 - a typical cross section for the borrow pit;
 - assumed quarry face profile approximately 45 degrees (°);
 - the borrow pit floor is excavated to a nominal depth but would in practice be inclined gently down slope into the excavation;
 - the maximum height of any single face would be no more than 12 m; and
 - drainage would be managed using a peripheral cut off ditch.

Proposed Borrow Pit BP01

- 1.4.9
- Proposed borrow pit BP01 is located within the south of the Site on the southern slopes of the Crooksetter hill formation, as shown on **Figure 2.2.1: Borrow Pit Location Plan** Peat cover of <0.5 m is locally present at this location based on the peat probe surveys undertaken.

Table 2.2.1: Proposed Borrow Pit BP01 (NGR 441627, 1174522)	
Borrow Pit Site Area	Maximum dimensions of search area: 118 m length 100 m width
Borrow Pit Search Area	11,800 m²
Borrow Pit Excavation Dimensions	Assumed dimensions: 90 m length 50 m width
Height of Excavation	12 m maximum
Area of Land Impacted	4,500 m² (Total Footprint incl. tie-in) 3,435 m² (Total Footprint excl. tie-in)
Slope Angle from DTM mapping	The slope angle of the search area is approx. 10°
Elevation of floor during construction	60 m AOD
Details of Extraction	No rock was observed within the borrow pit search area. As such, rock type, rock quality and weathering profile are all assumed. The assumptions are: - Drilling or Blasting required for Igneous rock due to high strength and likely discontinuity spacing. Hard ripping or blasting if metasandstones. - Orientation and spacing of discontinuities are unknown, As such a 45° angle of repose is assumed for the faces of the excavation.
Overburden Type and Depth	Superficial deposits during the peat probing survey recorded a maximum depth of 0.3 m of peat in this location, an overburden of less than 0.5 m is assumed.

Table 2.2.1: Proposed Borrow Pit BP01 (NGR 441627, 1174522)	
Indicative volume of aggregate extraction	Approximate volume of 24,000 m³ once 20% reduction applied.
Aggregate Composition	Assumed coarse grained granodiorite based on BGS mapping.

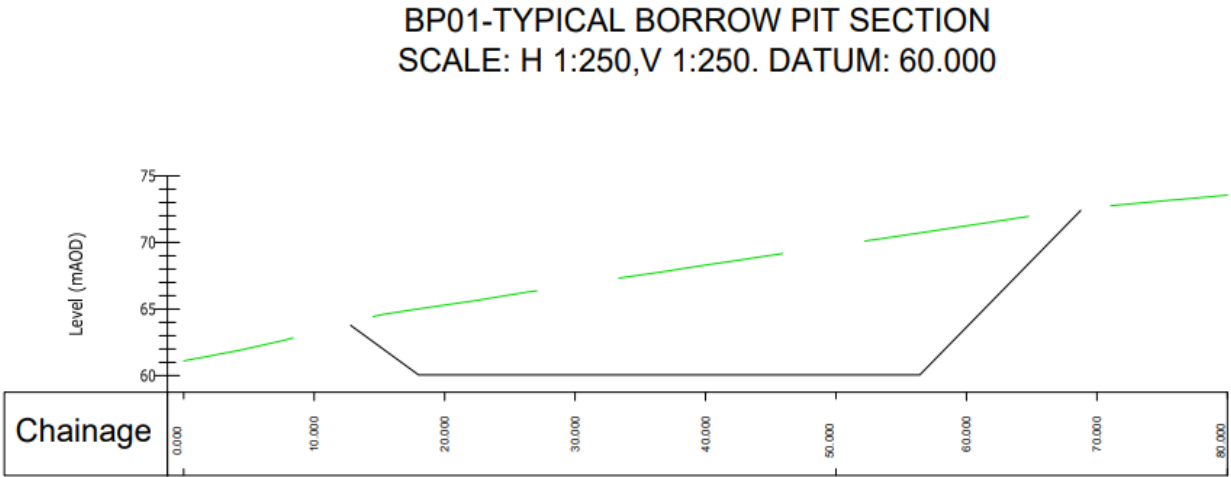


Figure 1: BP01 Typical Borrow Pit cross section

1.5 Summary

- 1.5.1 No exposures of bedrock were observed during the walkovers across the Site within the proposed borrow pit location. As such, assumptions have been made based on the published BGS mapping data¹ and the Site setting (slope angles and ground cover). Won materials within the Site would likely comprise of igneous granodiorite rock. A detailed assessment to determine the suitability of the rock would be required to confirm the exact extraction methods based on the intrusive site investigation data⁶.
- 1.5.2 Indicative aggregate volumes from the proposed borrow pit is assumed to be in the order of 24,000 m³ based on the dimensions and levels provided in **Table 2.2.1**. However, this would depend on a number of factors including:
 - results from the detailed design and intrusive investigation work prior to extraction including volume, quality and quantity of rock available for extraction at each location; and
 - potential visual impacts at each location.
- 1.5.3 It is estimated that the volumes of material available from the borrow pit location would not provide sufficient material for all construction requirements for the Proposed Development. However, detailed analysis of the rock quality for reuse as structural fill would be required following ground investigation.

1.6 Construction Requirements

Extraction Operations

- 1.6.1 The requirement to produce various grades of aggregate would necessitate the use of mobile plant and equipment. This operation would comprise of a few different elements which are summarised below.

Excavation of Materials
- 1.6.2 Drilling and blasting and chemical splitting is envisaged to be the methodology required for extraction of materials based on the likely strength assessment and discontinuity spacing of the assumed rock within the proposed borrow pit location. Rock samples should be taken for strength testing by an approved geotechnical laboratory to derive point load and Unconfined Compressive Strength (UCS) values. The contractor may wish to re-evaluate any alternatives to the requirement for digging on the basis of the available rock quality data.

Initial Stripping and Preparation
- 1.6.3 The initial access routes to the borrow pit would need to be constructed prior to the introduction of the main items of excavation plant and crushing/grading machinery.
- 1.6.4 It is anticipated that initial preparation would consist of a series of passes using an excavator with a blade along the final route of the temporary access track. This would have the effect of removing vegetation and any soft material, and also in compacting the weathered material located immediately above the bedrock. The gradient of the prepared access way would be no steeper than 1(V) in 10(H). The borrow pit would be accessed from the new track network. This process would require the section of track to be constructed from imported materials, unless further locally sourced suitable materials can be won during the preparation of founding levels for the wind farm infrastructure. In addition, the area of the proposed borrow pit would be required to be stripped of the superficial material including any soil which lies above bedrock. This material would need to be carefully lifted and placed in storage mounds within an appropriate storage area.

Crushing and Screening
- 1.6.5 The primary component of this operation would consist of a mobile crushing and screening system. Modern mobile crushing plants are available in a number of different formats and are usually available complete with screening capability. The contractor would need to provide a plant setup that meets the project requirements in terms of the ability to process the raw material, the quantities of the material required and the quality and size gradings of the product.
- 1.6.6 It is also envisaged that a rubber tyred front end loader would also be required in order to serve the crushing and stockpiling operation, as well as to produce loadout facilities for the truck and shovel based roadmaking operation.

Drainage
- 1.6.7 A drainage and surface water management system would be provided in order to control surface water runoff. Due to the relatively small size of any proposed excavation together with the associated plant site, the system would comprise of a peripheral cut-off ditch together with minor attenuation features or soakaways.
- 1.6.8 Given the low permeability and generally thin veneer of the overlying peat and superficial deposits it is not anticipated that groundwater ingress would be significant. However, the flow capacity of the bedrock

⁶ A revision of the graphical method for assessing the excavatability of rock, Pettifer and Fooks, Quarterly Journal of Engineering Geology and Hydrogeology 1994; v. 27; p. 145-164

would need to be determined to identify whether fracture flow is likely to be encountered and if standing water is likely to collect in the base of the excavation.

- 1.6.9 Water entering the borrow pits would need to be removed by either gravity drainage design or pumping depending on the overall morphology of the pit. The general topography in the areas identified is conducive to gravity drainage owing to the moderate to steep slopes. Discharge consent/EASR Permit may be required from SEPA for this activity. Water removed from the excavations would be passed through an appropriate sediment settling system to remove suspended sediment prior to discharge. The constructed drainage system and water pumped from the excavations would not be discharged directly to any natural watercourse.
- 1.6.10 It is not anticipated that volumes of groundwater that would require management would be encountered by the opening of the borrow pits at the Site due to the high elevations and slope angles. However, the groundwater regime would need to be verified through further ground investigation.

Environmental Management

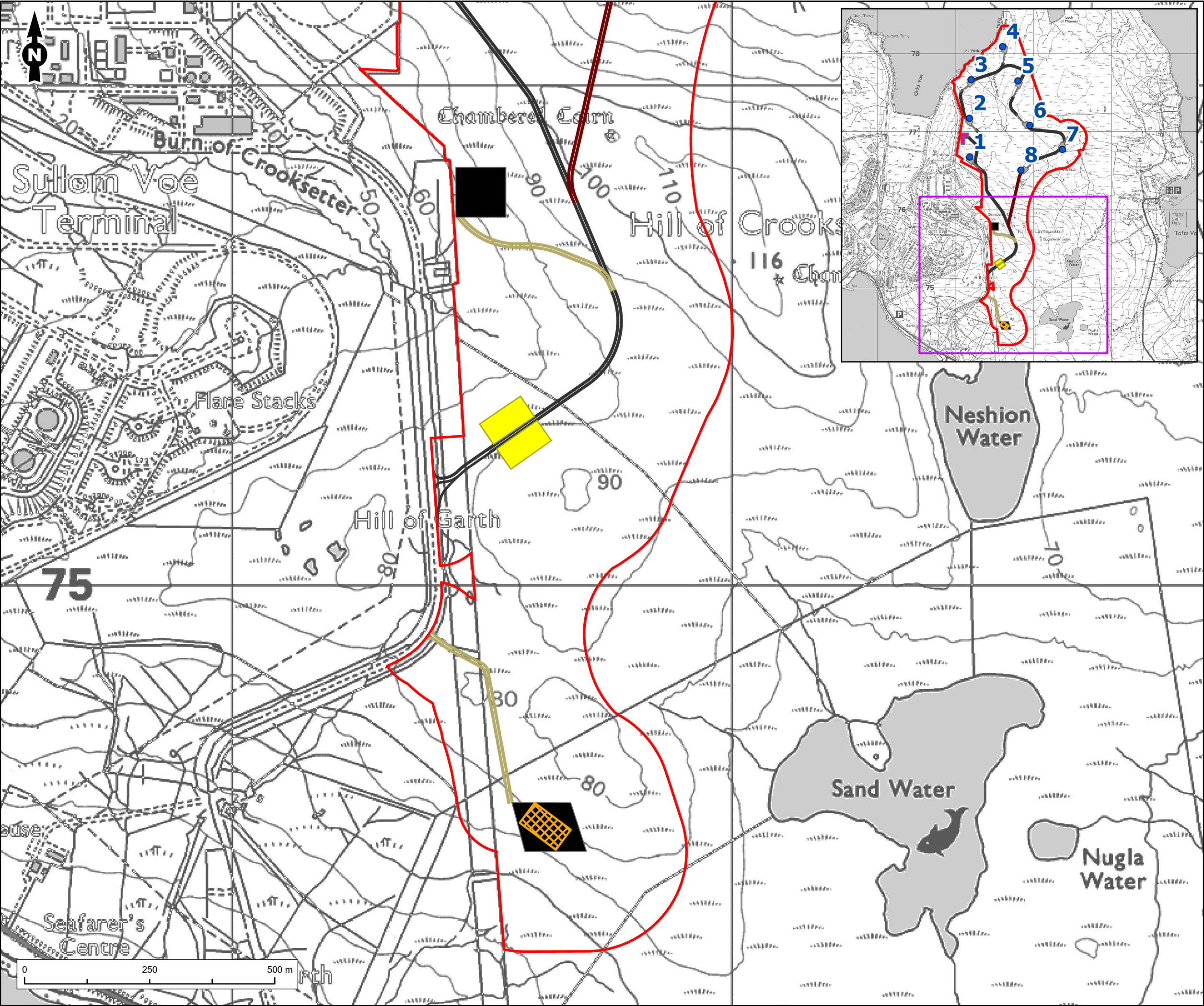
- 1.6.11 The Proposed Development would be designed, constructed, operated and decommissioned in line with relevant environmental legislation, guidance and good practice, to ensure that soils, and both groundwater and surface water are not contaminated.
- 1.6.12 During construction activities, a Construction Environmental Management Plan (CEMP) would be used to manage the potential impacts on the environment, and a specific plan covering borrow pits would be developed as part of the CEMP. An outline CEMP is presented in **Technical Appendix 2.1: Outline Construction Environmental Management Plan (OCEMP) (EIAR Volume 4)**. A detailed version would be produced by the appointed construction contractor post-consent (in accordance with the outline version) and sought for approval with the relevant planning authorities prior to the commencement of construction works.
- 1.6.13 Assuming good practice techniques are adhered to at all times and the implementation of mitigation measures as discussed above, it is anticipated that residual impacts from borrow pit activities on surface water, groundwater and soils would not be significant.

1.7 Conclusions and Recommendations

- 1.7.1 A reconnaissance walkover and supporting field surveys have been carried out within the Site to identify potential borrow pit locations. Two viable potential borrow pit search area locations were initially identified from desktop data analysis. Following the Site Walkover surveys, one borrow pit location was removed due to significant depth of peat cover. Therefore, this assessment is based on the remaining borrow pit location.
- 1.7.2 The surveys demonstrated that the areas of greatest potential in terms of bedrock excavation are located within the southern areas of the Site within the Graven Complex (Granodiorite) Formation. No existing borrow pits were observed within the Site.
- 1.7.3 The proposed borrow pit is likely to be predominantly coarse grained, igneous rock. No ground investigation has been undertaken within the Site to inform this assessment.
- 1.7.4 The proposed borrow pit is located on a slope with a slope angle of approximately 10° which may be excavated within a single layer of excavation. The overburden depths within the borrow pit search area are assumed to be less than 0.5 m and possess limited potential for peat cover.
- 1.7.5 The estimated amount of aggregate which could be won from the proposed borrow pit has been calculated as approximately 24,000 m³. This figure allows for a 20% reduction for unsuitable material or bulking of materials on excavation. This figure is not in excess of the estimated volume of aggregate required during the construction phase of the Proposed Development.

- 1.7.6 The primary use of aggregate arisings would be for the construction of tracks using unbound aggregate to the turbine suppliers' specifications and conforming to the Specification for Highways Works.

- 1.7.7 Detailed ground investigations, slope stability assessments and geotechnical testing would be required to inform the detailed design of the borrow pit to confirm the suitability of the material for use as part of the Proposed Development. It is anticipated that impacts on groundwater, surface water and soils from extraction of aggregate would not be significant, assuming use of good practice construction techniques and implementation of mitigation measures as set out in this document.



- Legend**
- Application Boundary
 - Proposed Turbine
 - Proposed Borrow Pit Location
 - Proposed Borrow Pit Search
 - Proposed Hardstanding
 - Proposed Substation, BESS and Lidar Area
 - Proposed Construction Compound
 - Proposed Operation and Maintenance Access Track
 - Proposed Access Track
 - Proposed Temporary Borrow Pit Access Track

Figure Title		
Borrow Pit Location Plan		
Project Name		
Neshion Energy Park		
Project No./Filyery ID		
1620016691 / REH2024N00248		
Date	Figure No.	Revision
March 2026	2.2.1	1.0
Prepared By	Scale	
FN	1:7,250 @A3	
Client		
Neshion Ltd		
		